RAILGUN APPLICATION FOR HIGH ENERGY IMPACT TESTING OF NANO-REINFORCED KEVLAR-BASED COMPOSITE MATERIALS

Micheli D., Vricella A., Pastore R., Morles RB., Marchetti M.

Sapienza University of Rome, Department of Astronautic, Electrical and Energy Engineering Via Salaria 851, 00138 Rome, (Italy) Email: davide.micheli@uniroma1.it

ABSTRACT

An advanced electromagnetic accelerator, called railgun, has been assembled and tuned in order to perform high energy impact test on layered structures. Different types of layered composite materials have been manufactured and characterized in terms of energy absorbing capability upon impact of metallic bullets fired at high velocity. The composite materials under testing are manufactured by integrating several layers of Kevlar fabric and carbon fiber ply within a polymeric matrix reinforced by carbon nanotubes at 1% of weight percentage. The experimental results show that the railgun-device is a good candidate to perform impact testing of materials in the space debris energy range, and that carbon nanotubes may enhance, when suitably coupled to the composite's matrix, the excellent antiballistic properties of the Kevlar fabrics.

1 INTRODUCTION

Carbon nanostructures (in particular nanotubes) are supposed to be ideal candidates as composite reinforcing filler, by means of their very low density (high surface area) joined to excellent mechanical properties. A scaled-up employment of such materials has been hindered so far by technical limitations related to their poor degree of bond to the macro-molecules of the conventional composites matrixes. Several chemical and morphological analyses have been carried out on the nano-reinforced composite materials before and after the ballistic characterization, in order to assess the effectiveness of the nano-filler in terms of impact resistance. In particular, viscosity and homogeneity of the enriched polymeric matrix are the main issues to be focused, as well as the physical coupling and the mechanism of the stress transfer to the Kevlar and carbon reinforcing fibers. In order to perform an high energy ballistic characterization of the manufactured composite samples an in-house built electromagnetic railgun was employed. A railgun is an electrically powered electromagnetic projectile launcher [1-4]. A railgun is made up of a pair of parallel conducting rails, along which a sliding metallic armature is accelerated

energy range, and that carbon nanotubes may enhance, when suitably coupled to the composite's matrix, the excellent antiballistic properties of the Kevlar fabrics. Further investigations on such topic are needed in order to achieve a better knowledge of the complex mechanism that drives the physical/chemical interactions between the carbon nanostructures and the fiber/matrix substrate during an high energy sharp external stress. Nevertheless, this work promotes the carbon nanotube employment in composite materials for aerospace applications, where the cogent constraints of lightweight and high mechanical resistance must be simultaneously satisfied. The paper is organised in three main sections. The first one describes the experimental activity focused on the manufacturing of layered composite structures. The second one analyses the inhouse built railgun. The last section reports some results about the firing tests carried out.

by the electromagnetic effect (Lorentz force) of a current that flows down one rail, into the armature and

then back along the other rail. The experimental results show that the railgun-device is a good candidate to

perform impact testing of materials in the space debris

2 MANUFACTURING OF LAYERED COMPOSITE MATERIAL

The composite materials under testing are manufactured by integrating several layers of Kevlar fabrics and carbon fiber ply within a polymeric matrix (epoxy resin) also reinforced by carbon nanotubes at 1wt% versus the matrix. The polymeric matrix is the bi-component epoxy resin PrimeTM 20LV (density 1.123 g/cm³) purchased at GURIT. The MWCNTs are the NC7000 (average diameter around 9.5 nm, average length 1.5 μ m, purity 90%, surface area 250-300 m²/g) supplied by NANOCYL. Fig.1 and Fig.2 show scanning electron microscope (SEM - TESCAN Vega 3LMH) pictures of the employed MWCNT. Four different kind of composite structures were manufactured: one by using only Kevlar fabric and epoxy resin, one by using only multiwall carbon nanotubes (MWCNTs) and epoxy resin, another one by using Kevlar fabric and carbon fiber embedded in the resin, and the last one by using

Proc. '6th European Conference on Space Debris'

Darmstadt, Germany, 22–25 April 2013 (ESA SP-723, August 2013)

Kevlar fabric, carbon fiber and by adding MWCNT as filler in the epoxy resin adopted to make the structure.



 SEM HV: 20.00 kV
 WD: 10.86 mm
 Little
 VEGAN TESCAN

 View field: 43.34 µm
 Det: SE
 10 µm
 Vefformance in nanospace

 SEM MAG: 50.00 kx
 Date(m/d/y): 07/15/10
 Performance in nanospace
 Figure 1. SEM pictures of MWCNT; pristine material.



Figure 2. SEM pictures of MWCNT. Zoom of one bundle of multiwall carbon nanotube; pristine material.

For each kind of structures two different thickness of the layered composite material were considered, one of about 3mm, and the other one of about 6mm. The first layered carbon fiber reinforced polymer (CFRP)+Kevlar

structure is made of three layers of carbon fiber (biaxial woven roving 0°-90°), taking care to overlap one layer upon the other by following the scheme (0°÷90°), (+45°÷-45°), (0°÷90°), two layers of biaxial Kevlar fabric, and again three layers of carbon fiber as above [5]. The second layered CFRP+Kevlar structure is made increasing the number of layers, exactly five layers of carbon fiber, three layers of biaxial Kevlar fabric, and again five layers of carbon fiber as above. In Fig.3, the first layered CFRP+Kevlar structure is shown. It can be observed the border parts of the manufactured structure before mechanical machining. In Fig.4, the first layered CFRP+Kevlar structure is shown after mechanical machining.



Figure 3. First kind of layered material. First layered CFRP+Kevlar structure before mechanical machining.



Figure 4. First kind of layered material. First layered CFRP+Kevlar structure after mechanical machining.

In Fig.5. a picture of both layered CFRP+Kevlar structures after mechanical machining is taken by showing one side of both sandwiches.



Figure 5. Picture of one side of the layered CFRP+Kevlar structures after mechanical machining.

It can be observed the different thickness of sandwiches: 3 mm and 6 mm respectively. In the second kind of layered materials MWCNT were homogeneously dispersed in the epoxy resin and such enriched resin was adopted to build Kevlar and carbon fiber layered composite materials. A critical issue of the nanoreinforced composite manufacturing is to perform the mixing of the nanoparticles within the matrix in such a way to obtain an homogeneous and isotropic distribution. Such requirement, needful for any kind of application, is critically hindered by the Van Der Walls forces that tend to aggregate the nanoparticles to each other [6-10]. Before mixing within the polymer matrix, the carbon nanomaterial was treated by sonication at room temperature in excess of ethanol. The sonication is carried out at 20 kHz for about 6 hours by means of Sonics Ultrasonicator (VCX750 model), setting 20% amplitude with respect to the full-scale oscillation magnitude of the ultrasonic processor. After this preliminary step, the resin is added to the alcoholic solution in such amount to have the desired MWCNT concentration in the final composite. The composite mixtures realized and analyzed consist in epoxy-resin with inclusion of MWCNT at 1wt% versus the matrix The obtained mixture is stirred for about 1h at room temperature, and then put in oven at ~60°C till the total evaporation of the solvent (typically it takes ~48h), finally an aminic hardener is added and mixed. To prepare the composite tiles, each layer is soaked within the mixture, then a pressure supplied by a load of about 50kg is applied over a square zone $(20 \times 20 \text{ cm}^2)$ of the multilayer. Finally, the resin curing process is applied in oven at a constant temperature (50°C for 16 hours).

In Fig.6, Fig.7 and Fig.8 the manufacturing of the MWCNT-reinforced layered structures is illustrated.



Figure 6. Manufacturing of nanostructured reinforced layered structures.



Figure 7. Top view of a nanostructured reinforced layered structures.



Figure 8. Picture of one side of layered CFRP+Kevlar structure after mechanical machining.

3 RAILGUN ANALISYS

In addition to military applications, railguns have been proposed to launch spacecraft into orbit [11-14]; however, unless the launching track was particularly long, and the acceleration required spread over a much longer time, such launches would necessarily be restricted to unmanned spacecraft. In the present work an electromagnetic launcher and in particular a railgun has been designed and manufactured. In Fig.9 the basic scheme of railgun is shown. The inner part made of two parallel barrel are the rails, while the remaining part are the mechanical assembly and the electrodes deputed to the energy supply.



Figure 9. Railgun scheme, the couple of rails are in blue colour.

y z x

y z



Figure 10. Mesh in numerical simulation of railgun by using finite element method.

The railgun length is 1m and the rails are electrically connected to a bank of 60 high voltage capacitors, for a total capacitance of about 5000 μ F. The capacitors can be charged up to 6500 V for a theoretical overall stored energy of about 100 kJ. A great effort has been provided in order to achieve a reasonable high level of ballistic test reproducibility, mainly for what concerns the control of the railgun bias parameters and their influence on both values and statistical dispersion of the output energy. The armature may be an integral part of the projectile (commonly called bullet), and the moving armature are referred to the projectile. The metallic bullets adopted to test the layered material samples are shown in Fig.11. The bullet armature is made of aluminium while the upper part of the bullet is made of tungsten.



Figure 11. Bullets pictures: the armature is made of aluminium while the upper part of tungsten.

In Fig.12 the in-house built railgun is shown. It can be observed the bank of capacitors and the electrical connections to the railgun.



Figure 12. Bank of high voltage capacitors electrically connected to the railgun.

The railgun has been numerically simulated by COMSOL Multiphysics finite element method (FEM) software analysis [15]. Determination of the magnetic flux density and current density has been computed for a supply voltage of 6 kV.





Figure 13. Railgun COMSOL simulation: computation of magnetic flux density (up), computation of current density (down).

In Fig.13, the simulation at the instant when the bullet is in the middle of its course between the rails is shown. Under these condition of magnetic flux density and current density the Lorentz force acting on the bullet is able to accelerate the bullet to values of velocity of thousands of m/s.

4 RESULT

In this last section some preliminary reports of the firing tests are illustrated. Three different test are shown, all for a capacitors charging voltage of 4kV: the first one on the material made by epoxy resin and Kevlar fabric, the second one on the material made by epoxy resin and MWCNTs, and the third one on the material made by

Kevlar fabric and carbon fiber ply, by adding MWCNT as filler in the epoxy resin adopted to make the layered composite structures. In Fig.14 the velocity of the bullet is shown. This measurement of velocity was computed by using a ballistic chronograph (CHRONY, able to measure velocities of bullet up to 2500 m/S).



Figure 14. Bullets velocity of 1100 m/s at 4000 V of capacitors charging voltage.



Figure 15. Damages of Kevlar based materials: sample front side (up), back side (down).

In Fig.15 the damage due to the impact on the material made exclusively by epoxy resin and Kevlar fabric is shown. In Fig.16 up to Fig.21 a sequence of pictures taken during the firing test on the nanostructured material made exclusively by epoxy resin and MWCNT is shown. It can be noticed the tile before firing in Fig.16 and the same after firing in Fig.21. In Fig.17-20 the plasma emission from the railgun in a 2ms of time-window and the intense flesh of light captured by the videocamera can be observed. The zero-instant photo is not reported, because at the start of the railgun fire the electromagnetic impulse (EMP) [16], generated by the extreme value of currents density, has induced some electromagnetic interference (EMI) [9] in the videocamera equipment affecting the quality of pictures.



Figure 16. Railgun ready to fire and material to be tested.



Figure 18. Railgun instants 2 of fire last 2ms.



Figure 19. Railgun instants 4 of fire last 2ms.



Figure 17. Railgun instants 1 of fire last 2ms.



Figure 20. Railgun instants 5 of fire last 2ms.



Figure 21. After the ballistic test the materials is completely destroyed.

In Fig.22 some bullets after firing tests are shown. It can be noticed the effect of currents. The mass of bullets decreases from about 19 to 14 g and from about 13 to about 9 g.



Figure 22. Two bullets after the firing test.

In Fig.23 and Fig.24 some pictures of the impact test on a tile made of Kevlar fabric, carbon fiber and MWCNT-reinforced epoxy resin are shown.



Figure 23. Damages of nanostructured Kevlar CFRP layered materials.



Figure 24. Damage of nanostructured Kevlar CFRP layered materials, zoom.

The results of this layered materials seems promising, since no extended damages has been discovered except of a little hole on the surface of structure. Further investigations, in order to achieve a better knowledge of the mechanism of the impact phenomena, as well as of the complex role of the carbon nanostructure in the load transfer to the carbon and the Kevlar fibers.

5 CONCLUSION

The paper analysed the effects of impact of metallic projectile on different type of composite materials. Tests were conducted by an in house railgun appositely manufactured for ballistic testing of materials at high energy of impact. Preliminary results show that the most promising materials able to resist to high velocity impact are nanostructured layered composite structures made by laminating several layer of carbon fiber, Kevlar fabric and by dispersing carbon nanotube in the epoxy resin adopted for the composite manufacturing.

6 **REFERENCES**

- R. Marshall, (1981). Railgun energy stores and systems, *in Proc. IEEE Int. Pulsed Power Conf.* pp. 193–196.
- J. V. Parker, (1982). Electromagnetic projectile acceleration utilizing distributed energy sources, J. Appl. Phys., 53(10), 6710–6723.
- 3. J. V. Parker, (1989). Why plasma armature railguns don't work and what can be done about it, *IEEE Trans. Magn.*, 25(1), 418–424.
- Micheli, D., Gradoni, G., Pastore, R., Apollo, C., Marchetti, M., (2010). Ballistic characterization of nanocomposite materials by means of "Coil Gun" electromagnetic accelerator, *ICEM 2010 Roma- XIX International Conference on Electrical Machines*, *IEEE Industrial Electronics Society (IEE)*. 1-6.
- Micheli. D., Laurenzi. S., Mariani Primiani V., Moglie F., Gradoni G., Marchetti M., (2012). ELECTROMAGNETIC SHIELDING OF ORIENTED CARBON FIBER COMPOSITE MATERIALS. ESA Workshop on Aerospace EMC, Venice, (Italy). 1-5.
- D. Micheli, R. Pastore, C. Apollo, M. Marchetti, G. Gradoni, V. Mariani Primiani, F. Moglie. Broadband Electromagnetic Absorbers Using Carbon Nanomaterial-Based Composites, (2011). *IEEE Trans. Microw. Tech.* 59(10), 2633-2646.
- F. Moglie, D. Micheli, S. Laurenzi, M. Marchetti, V. Mariani Primiani, Electromagnetic shielding performance of carbon foams, (2012). *Carbon* 50(5), 1972–1980.
- Davide Micheli, Carmelo Apollo, Roberto Pastore, Ramon Bueno Morles, Susanna Laurenzi, Mario Marchetti, (2011). Nanostructured composite materials for electromagnetic interference shielding applications", *Elsevier, Acta Astronautica*, 69(9–10), 747–757.
- D. Micheli, C. Apollo, R. Pastore, D. Barbera, R. Bueno Morles, M. Marchetti, G. Gradoni, V. Mariani Primiani, and F. Moglie, (2012) . Optimization of Multilayer Shields Made of Composite Nanomateriald Materials. *IEEE Trans. Electromagn. Compat.* 54(1), 60-69.
- D. Micheli, C. Apollo, R. Pastore, M. Marchetti, (2010). X-Band microwave characterization of carbon-based nanocomposite material, absorption capability comparison and RAS design simulation. *Compos. Sci. Technol.* 70(2), 400-409.
- 11.P. Lehmann, B. Reck, M.D.Vo, and J. Behrens, (2007). Acceleration of a Suborbital Payload Using

an Electromagnetic Railgun. *IEEE TRANSACTIONS* ON MAGNETICS. 43(1), 480 – 485.

- Palmer and R. Lenard, (1991). A revolution in access to space through spinoffs of SDI technology. *IEEE Trans. Magn.* 27(1), 11–20.
- 13. R. McNab, (2003). Launch to space with an electromagnetic railgun. *IEEE Trans. Magn.* 39(1), 295–304.
- 14. E. Schmidt and M. Bundy, (2005). Ballistic launch to space, in *Proc. 22th Int. Ballistic Symp.* 243–250.
- 15. R.W. Pryor, (2009). Multiphysics Modeling Using COMSOL: A First Principles Approach, *Jones & Bartlett Learning*.
- 16. Xijun Zhang, Jie Yang; Qingyun Yuan; Zhenxing Wang; Xianjun Li, (2011). Research on the suppressing behaviour of EMP protection device. Cross Strait Quad-Regional Radio Science and Wireless Technology Conference (CSQRWC). 1, 318 321.