



REACTION WHEEL SCARAB/PAMPERO

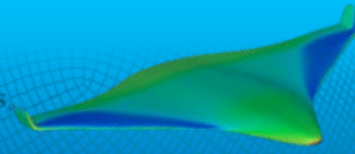
R.Tech

November 23th 2020

PR-RW-PRES-201120-2844-RTECH



$$\begin{aligned} \frac{\partial \mathcal{L}}{\partial y} + \text{div}(\rho \mathbf{u}) &= -\frac{\partial p}{\partial z} + \text{div}(\mu \nabla \mathbf{u}) \\ \text{div}(\rho \mathbf{u}) &= -p \text{div} \mathbf{u} + \text{div}(k \text{grad } T) + \Phi + S \end{aligned}$$



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The French Space Operation Act (2008) enforces the assessment of prospective risks

CNES is in charge of ensuring the right application of the law

CNES develops its own certification tool and spacecraft-oriented tools

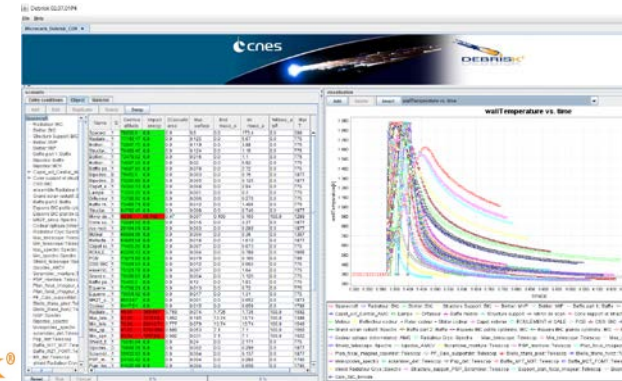
DEBRISK and PAMPERO





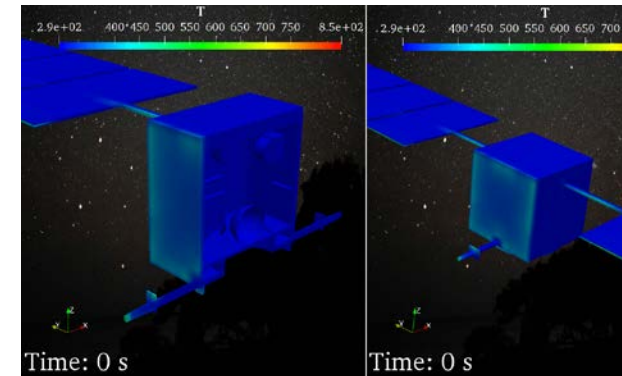
DEBRISK : French certification tool (100% CNES)

- Provided to the aerospace companies and operators
- Designed to perform **rapid survivability analyses** of fragments from space vehicles during their atmospheric reentry
- Based on an **object-oriented** approach



PAMPERO : French spacecraft-oriented tool (100% CNES)

- Validate assumptions used in object-oriented tools
- Perform computations for sensitive objects reaching the ground close to the 14J limit
- Perform computations for very **complex objects** (not available within object-oriented tools)
- Perform **D4D computations** for future missions
- Support **experts** for the **fragmentation** modelling
- Since 2020, R.TECH has an **exclusive license** of PAMPERO in order to achieve state of the art studies for customers of the industry

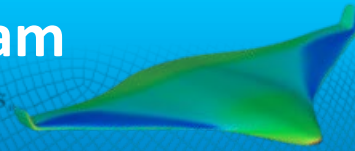




R.Tech

Research & Technology

PAMPERO Team



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Julien Annaloro
Project manager of PAMPERO



Martin Spel
Development Management



FR

NL

Eddy Constant
Engineer (PhD) Manager,
Thermal, aerothermal, Mechanical



Pierre van Hauwaert
Engineer, Architecture, Degradation/breakup
Aerothermodynamics, Meshing



J romine Dumon
Engineer (PhD),
Flight dynamics/Meshing



Valentin Ledermann
PhD student, Mechanical coupling



Iko Midani
PhD student, Aerothermodynamics

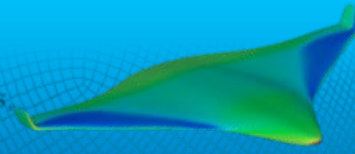


Philippe Makowski
IT support, testing and quality
assurance





$$\frac{\partial T}{\partial y} + \text{div}(\mu \text{ grad } w) =$$
$$+ \text{div}(\rho \mathbf{u}) = - \frac{\partial p}{\partial z} + \text{div}(\mu \text{ grad } w) + S_M$$
$$\text{div}(\rho \mathbf{u}) = - p \text{ div } \mathbf{u} + \text{div}(k \text{ grad } T) + \Phi + S$$



1 – Geometry and mesh

2 - Validation

3 – Results

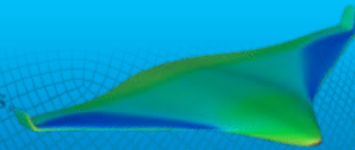
4 – Discussions



R.Tech

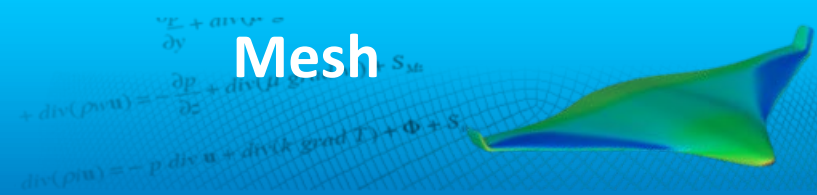
Research &
Technology

Geometry



Geometry :

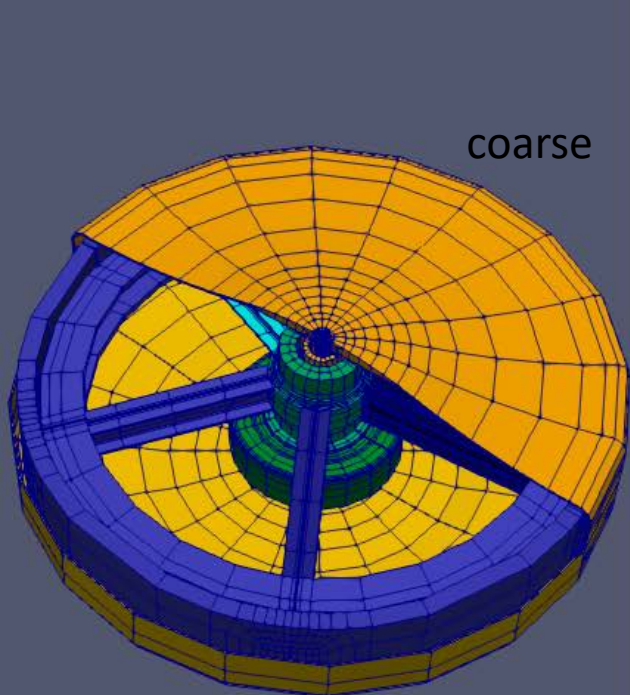
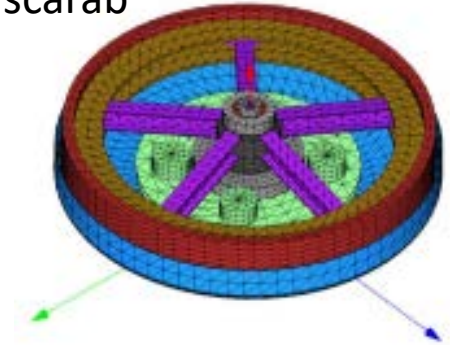
- Total mass : 7,79 kg



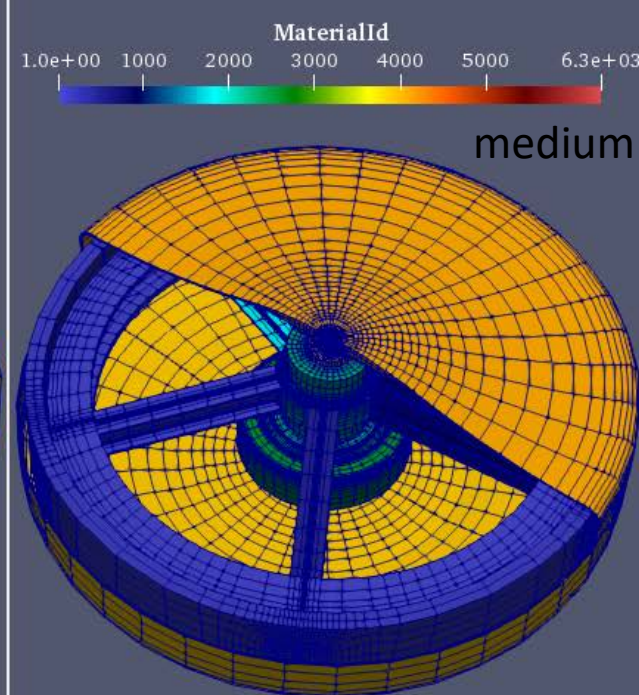
3 meshes :

- coarse : 7 303 cells
- medium : 59 144 cells
- fine : 199 611 cells

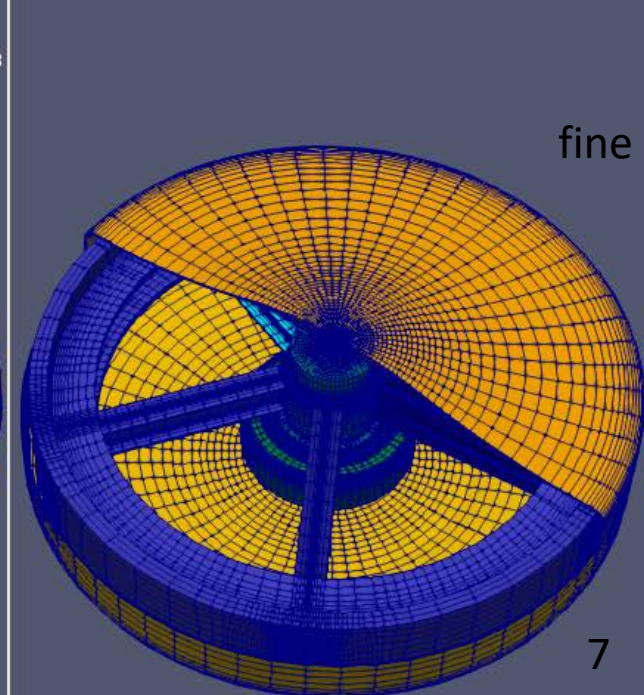
scarab



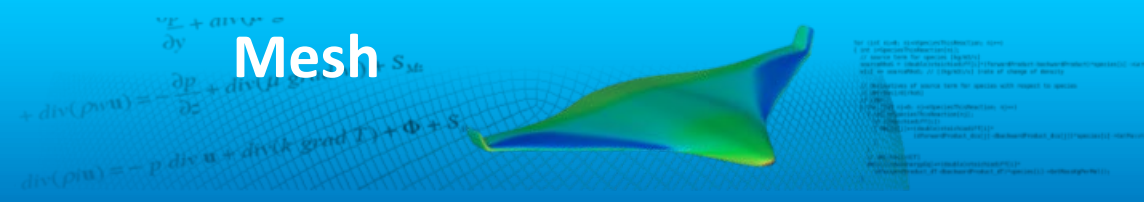
coarse



medium



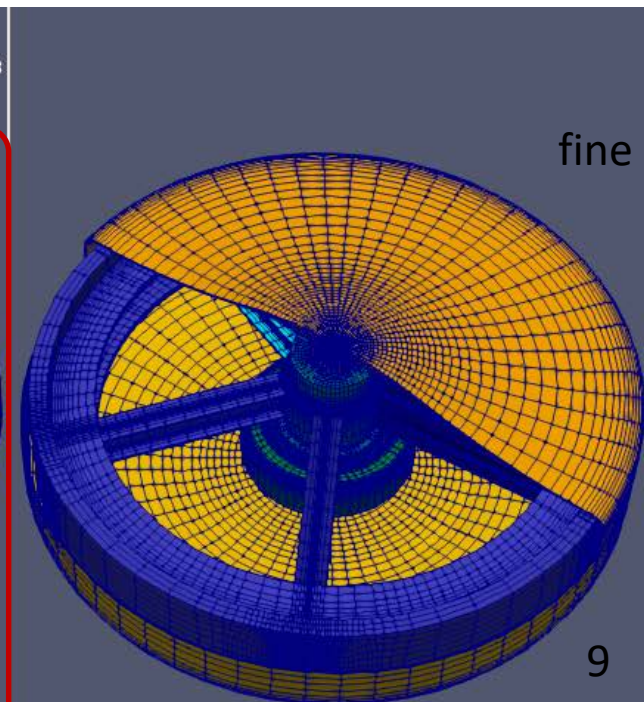
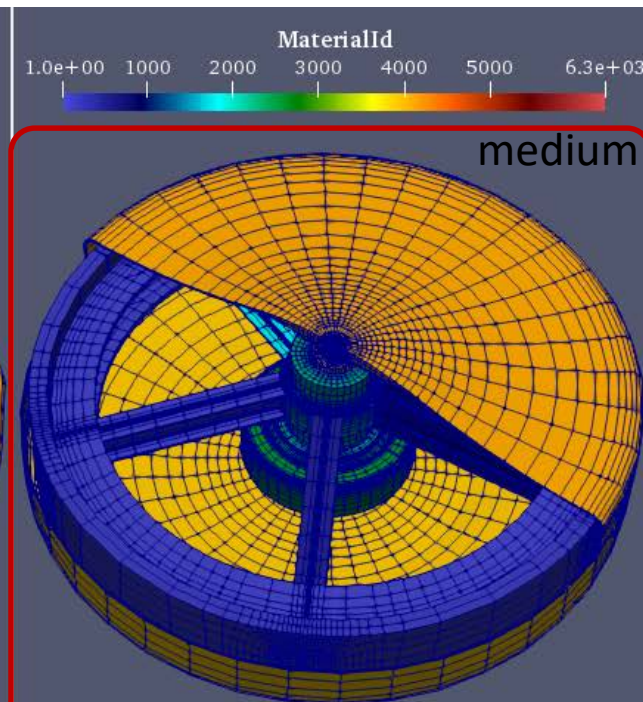
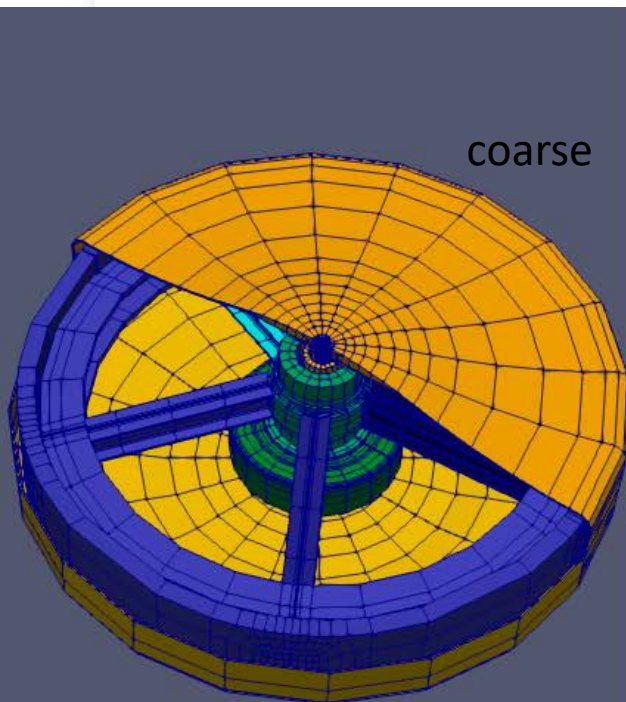
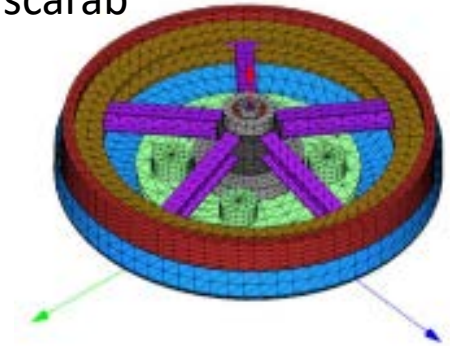
fine



3 meshes :

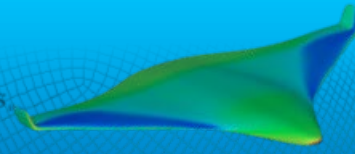
- coarse : 7 303 cells
- **medium : 59 144 cells**
- fine : 199 611 cells

scarab





$$\frac{\partial T}{\partial y} + \text{div}(\mu \text{ grad } w) = S_{M1}$$
$$+ \text{div}(\rho \mathbf{u} \mathbf{a}) = - \frac{\partial p}{\partial z} + \text{div}(\mu \text{ grad } w) + S_{M1}$$
$$\text{div}(\rho \mathbf{u}) = - p \text{ div } \mathbf{u} + \text{div}(k \text{ grad } T) + \Phi + S$$



1 – Geometry and mesh

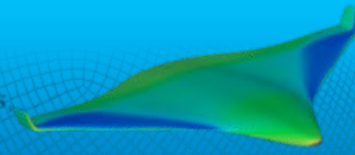
2 - Validation

3 – Results

4 – Discussions



Validation Low speed



Validation of the drag coefficient/ pressure distribution capture at low speed :

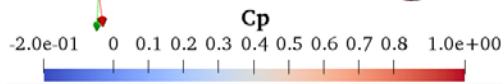
Very important to **insure a great accuracy** on the **impact energy** that could influence the **casualty area** of the debris.

Good match between PAMPERO, the CFD code OPENFOAM and experiments for different generic debris

PAMPERO



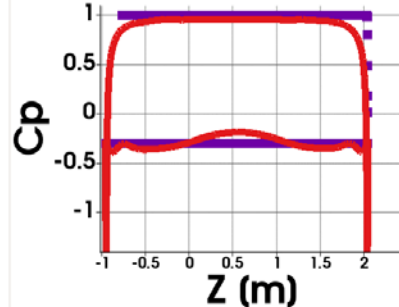
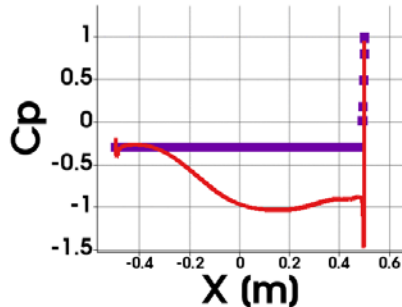
OpenFoam



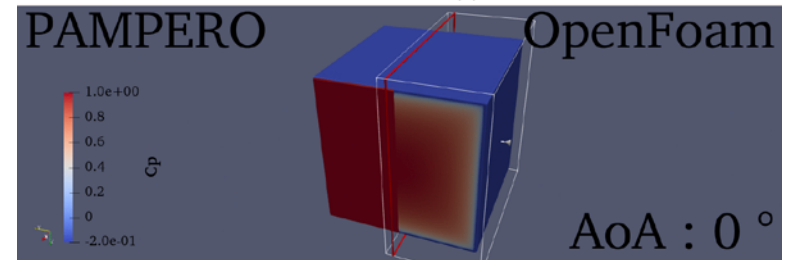
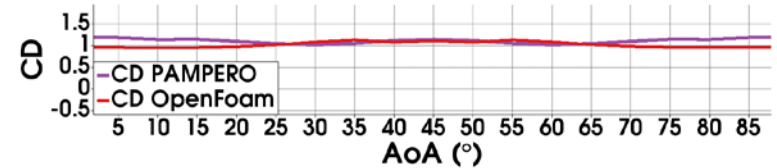
AoA : 0 °

Y = Z = 0

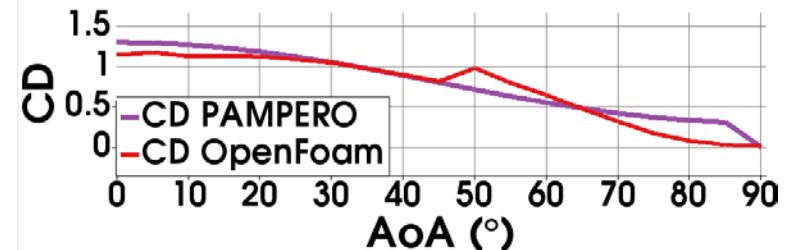
Y = X = 0



Pressure comparison over a cylinder at low speed with PAMPERO and OPENFOAM



Drag coefficient comparison (CD) over a cube at low speed with PAMPERO, OPENFOAM and experiments (*)



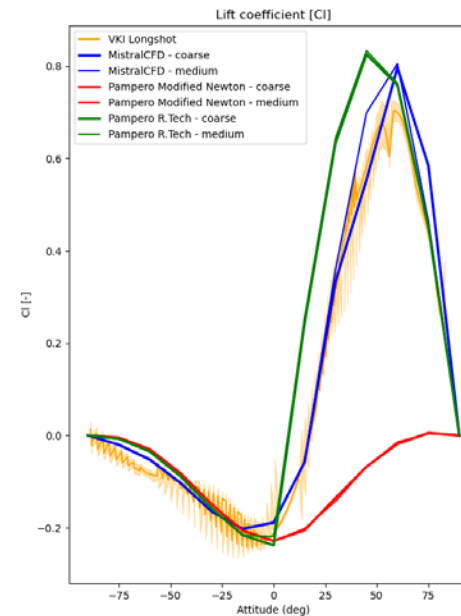
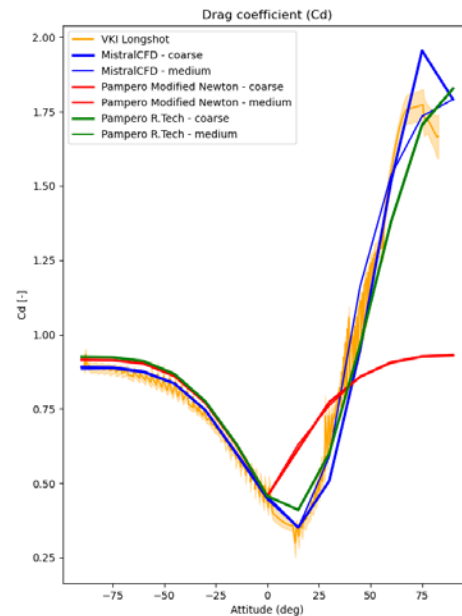
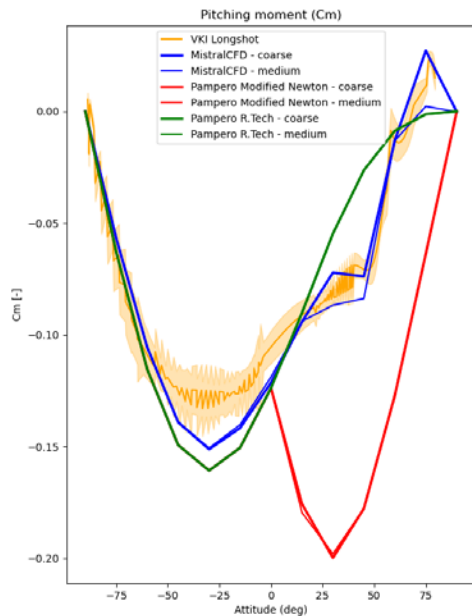
Drag coefficient comparison (CD) over a plate at low speed with PAMPERO, OPENFOAM and experiments (*)

Improvement to the Modified Newton method

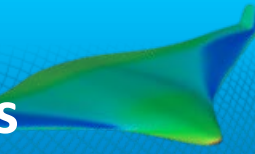
Automatic identification of concave regions

Validation of the aerodynamic coefficients on a concave shape very challenging for simplified aerodynamics softwares (concave shapes, unsteady phenomena)

Better agreement of PAMPERO with a CFD code (MISTRAL) and experiments (VKI Longshot)



J Annaloro, S. Galera, C Thiebaud, Martin Spel, Pierre Van Hauwaert, G G, S P, O C, P O Aerothermodynamics modelling of complex shapes in the DEBRISK atmospheric reentry tool: Methodology and validation, Acta Astronautica, Volume 171, 2020, Pages 388-402



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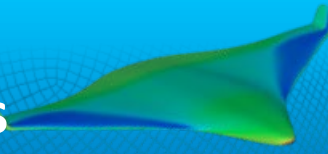
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Released conditions :

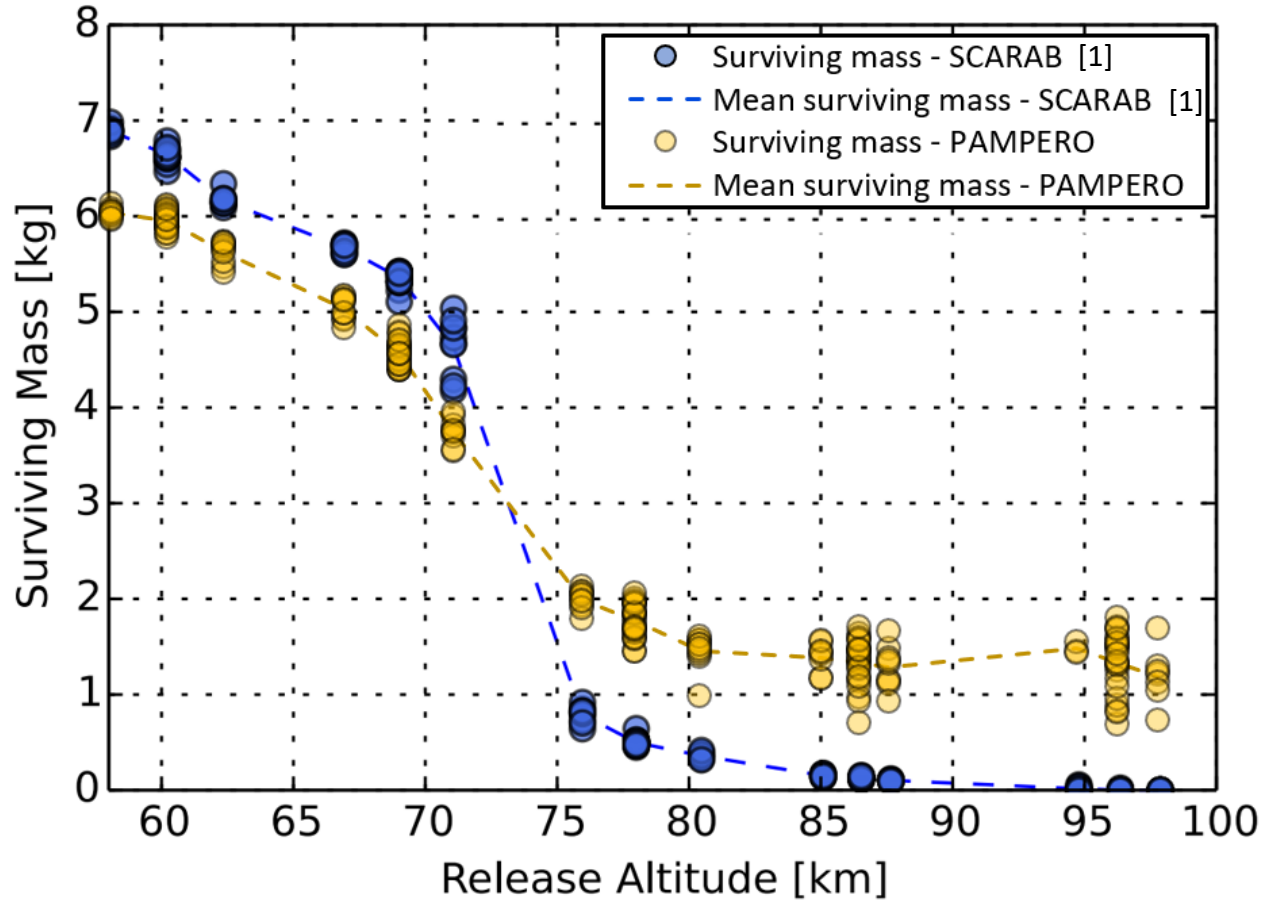
5 main altitudes with 25 attitudes

For each altitudes, 2 secondary altitudes with 10 attitudes each

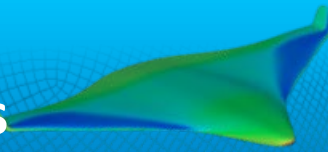
	→ 97,9 km	-----	10 cases attitudes varying	}	225 cases
96,4 km	-----	-----	25 cases attitudes varying		
→ 94,8 km	-----	-----	10 cases attitudes varying		
	→ 87,7 km	-----	10 cases attitudes varying		
86,5 km	-----	-----	25 cases attitudes varying		
→ 85,1 km	-----	-----	10 cases attitudes varying		
	→ 80,5 km	-----	10 cases attitudes varying		
78 km	-----	-----	25 cases attitudes varying		
→ 76 km	-----	-----	10 cases attitudes varying		
	→ 71,1 km	-----	10 cases attitudes varying		
69 km	-----	-----	25 cases attitudes varying		
→ 66,9 km	-----	-----	10 cases attitudes varying		
	→ 62,3 km	-----	10 cases attitudes varying		
60,2 km	-----	-----	25 cases attitudes varying		
→ 58,1 km	-----	-----	10 cases attitudes varying		



Surviving mass :



[1] P. Kärräng, T. Lips, T. Soares, Demisability of critical spacecraft components during atmospheric re-entry, 69th International Astronautical Congress, 2018



Casualty area (CA) :

- Casualty area – SCARAB [1]
- Mean casualty area – SCARAB [1]
- Casualty area – PAMPERO
- - - Mean casualty area – PAMPERO

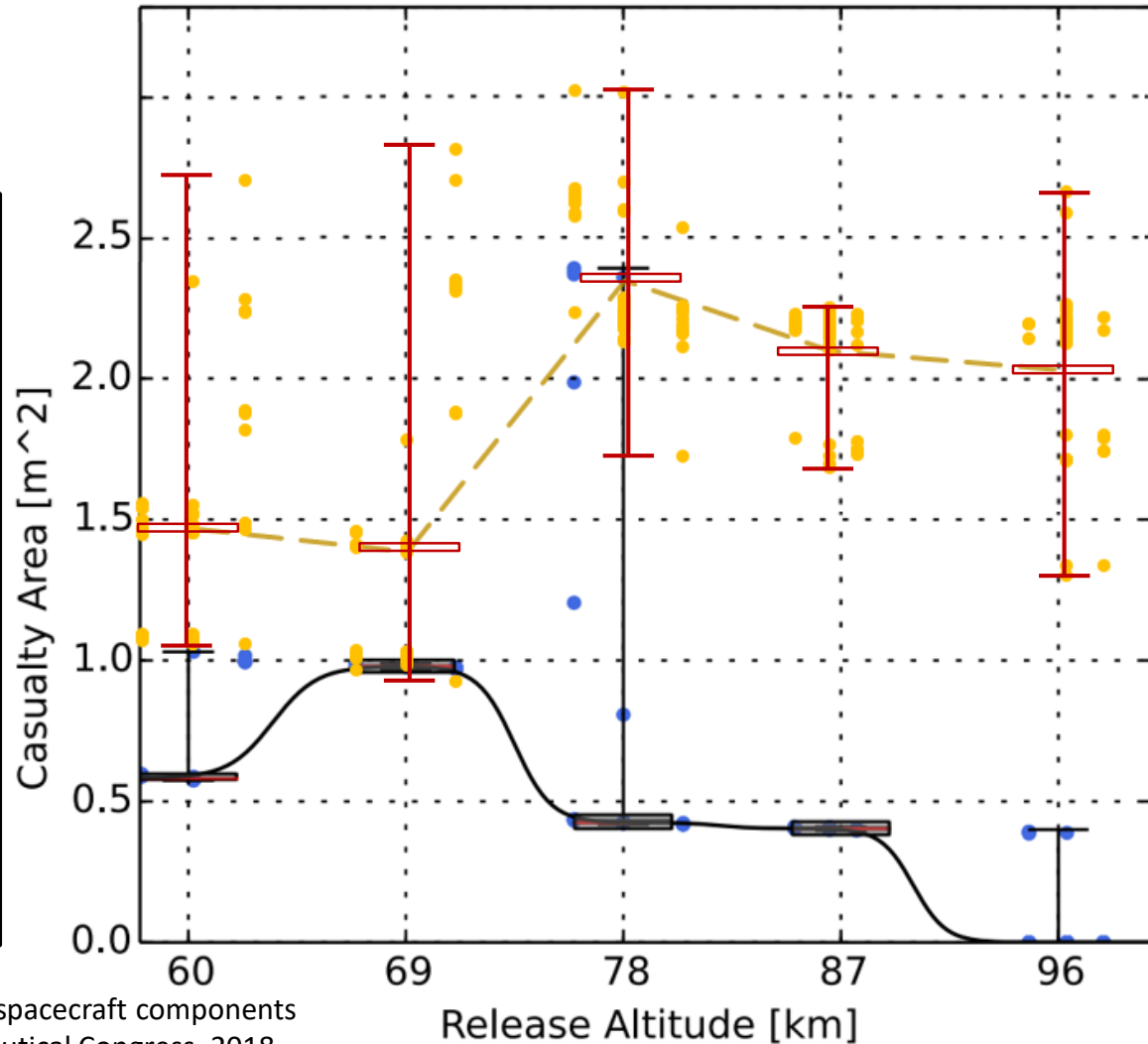
Results for 45 cases of the main and secondary altitudes :

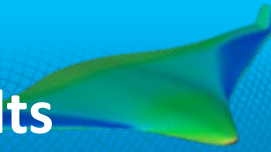
SCARAB : [1]

- ⊢ Maximal CA
- ⊢ Mean CA
- ⊢ Minimal CA

PAMPERO :

- ⊢ Maximal CA
- ⊢ Mean CA
- ⊢ Minimal CA



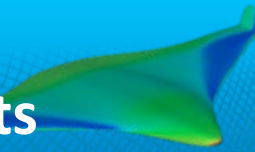


Ground fragments for 25 cases :

- Altitude = 96,4 km
- Variable : attitude

	A	B	C	D	E	F	G	H	J	K	L	M
How many times (out of 25) these parts are found on ground ? Mean surviving mass [kg, % of initial mass] ?												
Impact probability	0	25 %	1	100 %	0	0	0	0	4 %	4 %	4 %	0
Surviving mass [kg]		$1.89 \cdot 10^{-3}$	$1.16 \cdot 10^{-5}$	1,306					$8.84 \cdot 10^{-2}$	$1.39 \cdot 10^{-1}$	$9.81 \cdot 10^{-4}$	
% of initial mass		12 %	0 %	32 %					49 %	65 %	0,6 %	

- Most popular on ground :
 - D in steel (initial mass = 4,1 kg)
 - B in titan (initial mass = 16 g)

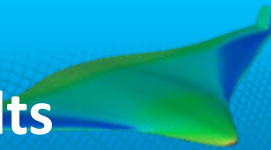


Ground fragments for 25 cases :

- Altitude = 86,5 km
- Variable : attitude

	A	B	C	D	E	F	G	H	J	K	L	M
How many times (out of 25) these parts are found on ground ? Mean surviving mass [kg, % of initial mass] ?												
Impact probability	0	40 %	0	100%	0	0	0	0	0	0	0	0
Surviving mass [kg]		5.34 10 ⁻⁴		1,342								
% of initial mass		3 %		33%								

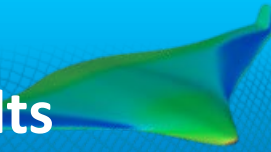
- Two parts on ground :
 - D in steel (initial mass = 4,1 kg)
 - B in titan (initial mass = 16 g)



Ground fragments for 25 cases :

- Altitude = 78 km
- Variable : attitude

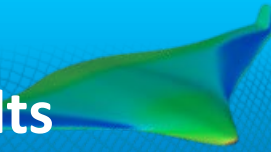
	A	B	C	D	E	F	G	H	J	K	L	M
How many times (out of 15) these parts are found on ground ? Mean surviving mass [kg, % of initial mass] ?												
Impact probability	0	0	0	100 %	0	0	0	13 %	0	0	0	20 %
Surviving mass [kg]				1.747				0.003				0.006
% of initial mass				43 %				0,4 %				2 %



Ground fragments for 25 cases :

- Altitude = 69 km
- Variable : attitude

	A	B	C	D	E	F	G	H	J	K	L	M
How many times (out of 24) these parts are found on ground ? Mean surviving mass [kg, % of initial mass] ?												
Impact probability	4 %	0 %	0 %	100 %	0 %	100 %	0 %	100 %	79 %	83 %	87 %	100 %
Surviving mass [kg]	0.022			3.830		0.123		0.375	0.007	0.025	0.013	0.115
% of initial mass	5 %			94 %		27 %		49 %	4 %	12 %	8 %	42 %



Ground fragments for 25 cases :

- Altitude = 60,2 km
- Variable : attitude

	A	B	C	D	E	F	G	H	J	K	L	M
How many times (out of 25) these parts are found on ground ? Mean surviving mass [kg, % of initial mass] ?												
Impact probability	52 %	100 %	36 %	100 %	28 %	100 %	56 %	100 %	100 %	100 %	100 %	100 %
Surviving mass [kg]	0.022	0.015	0.029	4.075	0.017	0.158	0.043	0.747	0.165	0.154	0.168	0.264
% of initial mass	5 %	94 %	4 %	100 %	7 %	35 %	18 %	98 %	92 %	72 %	97 %	96 %



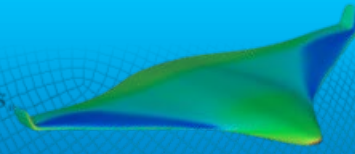
PAMPERO

cnes





$$\frac{\partial T}{\partial y} + \text{div}(\mu \text{ grad } w) =$$
$$+ \text{div}(\rho \mathbf{u}) = - \frac{\partial p}{\partial z} + \text{div}(\mu \text{ grad } w) + S_M$$
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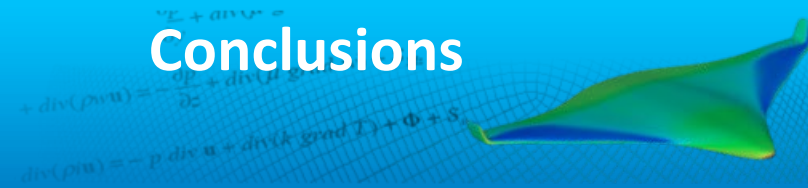


1 – Geometry and mesh

2 - Validation

3 – Results

4 – Conclusions



Conclusions

- Good agreement between SCARAB and PAMPERO results of the surviving mass evolution
- Differences more important for the casualty area
- Influence of the attitude more important with PAMPERO, results more dispersive
- Emissivity could be one of many causes of differences and more generally material data